

31 FB #17

#452 C.S. #209 sec. 20 1/8-10-7

Kays & Thowls & Martin - Dingman

MAY 28-1914

Begin at sec. cor S. sec. 20. Stone

Per J.A.G. A.W. Trevis N. 74° 40' W. 100'

Run West 121 1/2' correct 52.5 = 889' 08" W

- 5.00	5.00	5.00	
- 5.00 + 10'	4.924	9.924	
- 0.20	.200	10.124	
① 5.00 + 28'	4.415	14.539	
② 0.423	.423	14.962	S. 1226
③ 1.531 + 6'	1.819	16.781	S. 253
④ 3.700 + 1 1/2'	3.699	20.480	S. 309
⑤ 2.438 + 7 1/2'	2.403	22.883	S. 346
⑥ 3.745 + 3'	3.740	26.623	S. 1402
⑦ 1.225 - 10'	1.297	27.920	W. 1.034
⑧ 3.31 - 17 1/2'	3.160	30.970	L. 302 1/2' = L. 503' S. 06° 46' 12" E
⑨ 0.843 - 5'	0.836	31.806	L. 400' = L. 1000' S. 100' = S. 100' 252'
⑩ 3.325 - 11'	3.267	35.073	S. 216 55' 29" = 313
⑪ 1.740 + 5 1/2'	1.732	36.805	S. 247 = 553' .305
⑫ 1.035 - 3 1/2'	1.033	37.838	S. 268 53' 0" = 570
⑬ 1.936 - 14'	1.930	39.768	L. 36' 53" 70 80' = S. 299' S. 02' = 301
	.395	40.163	= 739' 10" S. 307 N. = 206 N
⑭ 453 - 16'	397.8	40.224	A 12 = W. 241 + N. 229
⑮ " " "	40.224	40.224	70.193
⑯ " " "	40.224	40.224	1091
⑰ 2.326 + 7 1/2'	2.306	2.613	E. 059
- 1.50 - 2'	1.799	4.412	E. 000
⑱ 3.149 + 7 1/2'	3.467	7.879	E. 096
⑲ 2.568 + 25 1/2'	2.594	10.473	E. 115
⑳ 153 + 17'	2.059	12.532	E. 129
㉑ 11.809 + 9'	1.291	13.823	E. 138
㉒ 2.817 + 4 1/2'	2.809	16.632	E. 158
㉓ 1.636 - 2 1/2'	1.634	18.266	E. 169 - set sub cor. 116 1/2' = E. 151
- 5.00 - 1'	4.963	23.229	
- 8.90 - 1 1/2'	3.833	27.064	
㉔ 6.336 + 5 1/2'	6.307	33.371	E. 276 30'
㉕ 616 - 6'	.552	33.923	E. 279 58' 40" 25' cor. E. 322
㉖ 3.253 - 20'	3.050	37.038	APPROX. cor. 600' S. 28° E. 60'
㉗ 3.520 - 13'	3.423	40.461	
- 2.600 + 16'	2.496	42.957	
- 1.200	1.200	44.157	
㉘ 4.000	4.000	48.157	
- 5.000 + 1 1/2'	5.000	53.157	1.50 + 1 1/2' = 1.50 + 57.609
- 1.200 + 1 1/2'	1.162	54.319	
㉙ 1.156	1.156	55.475	57.65 + 55.259

257	263	200	3007	181	304
286	282.53	75	75	42	063
259	259	3.085	3.085	017	362
134	8.4368002	999	98351	12	27
331	0.5798286	051	98256	37	27
617	9.9800122	988	00122	37	27
050	18.9366401	204	99678	3160	37
503	8.9446061	999	53114	056	37
543	9.9258287	922	58257	1074	37
655	9.9979964	999	79964	1139	37
073	25.5684303	199	22155	2559	37
100	8.2415500	326	7	056	37
796	0.9010225	173	24.999	057	37
1390	7.425772	105	3.6082	105	37
		183	2.962	139	37
		79	62.8358	146	37
		93	97	147	37
37	9.7885326	999	70254	025	37
50	9.6959703	969	89703	39897	37
307	19.4975020	195	99967	3946	37
				322	37
				041	37
28	9.6845775	994	20295	251	37
640	9.8061890	950	61805	39897	37
Cor 35	9.9991890	999	91890	48461	37
3092	29.4902561	297	47395	569	37
				39902	37
606	9.782473	160	4042	008	37
40.113	1.604042	999	9950	39824	37
52	8.178431	116	04092	40.188	37
				19.945	37
				15.266	37
				1.679	37
				240.183	37
				204.80	37
				204.50	37
				3.88	37
				1.44	37
				198	37
				40.224	37
				45.157	37
				55.259	37
				57.65	37
				19.26	37
				436	37
				225	37

Set 4 sec. cor. Cedar stake
 MARK. FIX. 24" S. 24 1/2° E. 1.115
 FIX. 14" S. 65 1/2° W. 2 1/4" stake 2.069

"B" cont. May. 29 - 1913

3.405-37	3398	59.165	E. 221
0.263	263	59.478	E. 217
3.200-24	2923	62.341	E. 204
5.000+20	4691	67.032	E. 177
1.440+10	1379	67.471	E. 177
5.000+25	4652	73.063	E. 147
1.300+15	1236	74.299	E. 140
2.000+15	1943	76.244	E. 131
3.300+6	3252	79.526	E. 120
	5494	79.521	
	2455	39.582	
	79.526	79.816	
		59.705	

Reestablish $15^{\circ} 17'$ Fir limb in old corner

Mark. Fir 24" N. $67^{\circ} E 3.19'$ Fir 5" $1.8^{\circ} E 1.247-3'$

Fir 20" N. $53^{\circ} 30' W 4.73-9'$ Mark taken about 40' high

C LIME 505 N. of true

From "B" N. $89^{\circ} 30' E$.

2.477+29302	151	2.151	N. 242
1.609+617	1592	2.743	N. 276
6.547-20	16879	12.646	N. 325
0.900-10	886	11.502	N. 249
0.400	400	11.902	N. 253
9.92-24	2723	14.623	N. 312
1.990-8	2961	17.586	N. 366
2.090-25	1845	19.431	N. 416
2.610-30	2267	21.692	N. 465
0.533	533	22.545	N. 482
1.907-113	1867	24.412	N. 523
1.609-152	1551	25.963	N. 556
A. 646-10	4576	30.539	N. 556
9.017	9017	39.556	N. 556

Fir Pt. 40' to Mark $3.514^{\circ} E 1.972'$

Set Δ 1/4 bears N. $20^{\circ} 11' E 97'$

Set Δ 1/4 near $\frac{1}{4}$ sec. corner $1235 N. 2009 W$

For translation base. Vertex is $1^{\circ} 14' N 9^{\circ} 50' - 15^{\circ} 42' - 210'$

Falls 244 S. correction $1^{\circ} 14' N N. 50^{\circ} E 3105$

11.5 E. 122
9.5 1.25
7.50
54.051
54.19
150.00
39.25
19.23
20.00
8.49

7.050	10.861	4.580
105.1235	0.0916	6.672
2.09	9.996	9.41
8.9706	10.957	8.190

5.14750	0.8655	3.000	0.0976	6.67
40.1235	0.0916	6.672	5.5742	2.12
2.09	9.996	9.41	8.6658	9.04
9.169	10.955	0.57		

7.50	0.8655	3.000	2.864
12.35	0.0916	6.672	4.52
2.09	9.996	9.41	0.60
9.255	10.956	5.913	4.27

8.9706	10.9525	8.190	3.22	3.00	2.25
			1.12	2.610	0.9
			2.10		2.261

2.744	9.667	7.76	9.947	0.04	2.79236
97	9.956	7.72	9.986	7.72	3.9.118
4.514	19.654	5.558	19.933	7.76	2.9.202
39.536					2.84

4.082					
8.6539	1.10	9.999	5.580	6.02	0.60
9.0492	1.8	9.0492	1.8	9.995	9.7
17.703	1.29	17.048	7.76	6.02	1.6

3.64	9.936	5.141	11.60	0.9	2.9
39.536	1.60	0.9	9.999	8.9	7.18
1.214	8.335	5.55	16.00	0.9	3.9.905

3.22	3.3				
2.24	3.3				
2.24	3.3				
2.24	3.3				

Set sub. loc. at $59.705 + E. 217$
Cedar stake Fir N. $60^{\circ} 2' W 9.63 - 20' = 5.87$

"F" Line S. thru 1/2 sec. 20

S. 0° 02' E. From "D" @ +750

① 2.70-5 $\frac{1}{2}$	2.672	2.672	
- 1.50-9 $\frac{1}{2}$	1.479	4.151	
- 5.00-5 $\frac{1}{2}$	4.951	9.132	
② 1.03-7 $\frac{1}{2}$	1.023	10.155	
③ 1.05-20 $\frac{1}{2}$	2.954	11.139	
④ 2.629-25 $\frac{1}{2}$	2.414	13.553	
⑤ 2.1700	2.506	15.853	
⑥ 3.520-5 $\frac{1}{2}$	3.494	19.347	
- 5.000-17 $\frac{1}{2}$	4.752	24.129	
⑦ 2.495-5 $\frac{1}{2}$	2.452	26.611	
⑧ 2.850+5 $\frac{1}{2}$	2.568	29.479	E. 14.
⑨ 1.464+24 $\frac{1}{2}$	1.329	30.808	E. 14.05
⑩ 1.744+17 $\frac{1}{2}$	1.661	32.469	E. 14.1
1.461+20	1.373	32.842	E. 14.2
⑪ 1.244+25 $\frac{1}{2}$	1.094	34.936	E. 14.2
⑫ 1.725+11 $\frac{1}{2}$	1.659	36.625	E. 14.3
⑬ 3.004+12 $\frac{1}{2}$	2.933	39.558	+ 0.06 Intersect at A. @ -244
		39.558	
		3.07	
		39.578	

"G" Line W. thru E. 20

Begin at "F" @ +1.214 S. 15° 43' W.

① 0.987+7 $\frac{1}{2}$	979	979	S. 10.02
② 2.904+3 $\frac{1}{2}$	2.899	3.878	S. 07.007
③ 1.965-7 $\frac{1}{2}$	1.948	5.826	S. 01.0
④ 3.880-18 $\frac{1}{2}$	3.690	9.516	S. 01.7
⑤ 3.540-11 $\frac{1}{2}$	3.466	12.982	S. 02.3
⑥ 2.400-6 $\frac{1}{2}$	2.356	15.368	S. 02.7
⑦ 4.525-6 $\frac{1}{2}$	4.009	19.877	F. 11.035 N. of cor
	19.877		

set. sub. cor. at "E" @ +1.214 ~ 054 E. Fir Limb

Fir 36" S. 21 $\frac{1}{2}$ ° E. 10.09 + 9 $\frac{1}{2}$

set. sub. cor. on S. 1. sec. 20. at A. ③ - ~ 309 N.

Cedar stake. Fir 24" N. 32° E. 807 - 16 $\frac{1}{2}$ ° 724

2352	2414	1464	1271	173	1619	9200	1316
2414	2414	1464	1329	1244	1667	1441	1373
2045	2045	2045	20153	20153	17° 3.880	3614	
20236	20236	20236	20236	20236	19.977	19.977	
20092	20092	20092	20092	20092	19.951	19.951	
7.264	7.264	7.264	7.264	7.264	20.068	59.705	
01056	01056	01056	01056	01056	39.894	39.894	
N	S	E	W				
19.975	19.975	02.26	124	10			
3.03	3.03	0.88	20.068	39.905	40.183		
20.258	20.258	20.167	20.202	40.177	39.905		
23.905	20.083	17	20.072	175	256	55	
19.953	322	14	158	186	268	20	
0.64	19.761	231	158	186	268	20	
19.888	17	152	175	186	268	20	
76.1	17	14	151	186	268	20	
1127							
39.905	28	47	19.962	19	186	20092	
071	247	180	19.900	14	198	192	
5.976	2.52	0.52	19.700	233	284	19.900	
40.183	0.42		19.700	162	192	19.761	
207.209			1.39			.139	
29.873	144	144	19.347				
27.883	132	144	614				
11.841	282	154	19.961				
0.40	2141	134	0.10				
19.951	2393	2347	19.971				
181	9.259679	0.225051	9.259679				
1679	0.225051	9.997493	9.997493				
6091	9.032628	0.227558	1689				

ATC² Turn Left 45° 45' 1.917 + 4°

Thence Angle L. 53° 26' to W. end of Δ Base

Angle is 6° 49'

Length of Base 4.788

interior Lot E. End of Base 85° 34'

" " " " " " 57° 38'

the cor. of secs. N5, 17 & 18. as tract

by J. P. Panone is 456 too far East

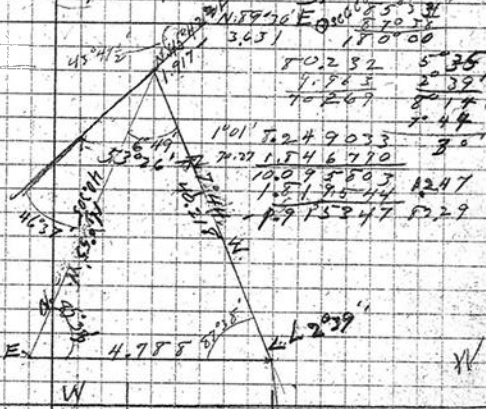
Move West 156 = Mark. Fir 30 N 57° E 139-172

Fir 26 N 89° E 96-177 Fir 24 S 44° W 869-15-264

TURN South Needle

① 1.695-50	1.692	1.692 E 184'
② 2.365-30	2.362	4.054 E 415'
③ 4.026+630	4.000	8.054 E 528'
④ 1.909-	1.909	9.963 to approx. 15.100 E 10.21
⑤ 457-	457	to vertex 5011' E. 10.65
2.1479-20°	2.329	12.791 E. 13W
4.500-226°	3.887	16.678 E. 17W
① 1.646	1.646	18.324 E. 18W
② 5.069-34°	5.011	23.385 E. 22.95
③ 4.338-	4.338	27.723 E. 28.21
④ 3.293-	3.293	31.016 E. 31.87
⑤ 3.017-	3.017	34.033 L. 5° 35' to W. end Δ Base E. 34.75
4.957	4.957	L. 6° 29' to vertex L. 58.411
set 4 sec. cor. 4 115' E. 143		4115'
set 33. 16X 10X 9" Mark. Fir 34 N 43° W. 302		2732'

230	549	648	100	200	157L
903	53030	46° 57'	32053	359	1155
1.397-172	45° 42'	45742	1.917	1204	2.078
200	7° 44'	65	790	90	2.580
2339			400		.189
			1.195		1.576
			1.576		1.185
			2.766		2.759
			2.58		2.580
			1.586		.179
			98826224		
N 79° 30' E. 99994045			99994045		
23643 475	207260103		207368706	613705	3743
45422	98441144		9854727	53706	112
1.917	0.2526224		02826224	13703	3.631
4	99994045		99994045		
1337	207261407		201367534	13705	86° 49'
1336				13705	86° 49'
1335				13705	86° 49'
1334				13705	86° 49'



N	S	E	W	
032		3631		N. 89° 30' E. 3.671
1339		1370		N. 45° 42' E. 1.917
39852			5412	N. 7° 44' W. 40.215
4938			439	N. 5° 00' S. W. 4.957
34023		297		N. 0° 30' E. 2.34033
70192		5297	5551	
			2550	
3079408427	30		79408427	
3631	2560026134033		15315625	
03164	5.5008685		9.4727046	
7449	1289250		99960322	
40218	16044197		16044197	
541210	73233449		11.6004510	39.852
				1.168
505	99474567		99982890	
4947	06952195		06952195	
4392	9642675		106935085	4938
505	998083		9997825	
4737	062219		0695219	
4523	9683302		106951544	4933
3183	502846			

201182 80192
40086 40166
49076

36

#209

I Litta Withrd sec. 18.

N. 87°40' W.

① 2.386+28°	2.097	2.097	S. 018 = 119'
② .972+14°	.943	3.040	S. 026 = 172'
③ 2.772+14°	2.658	5.728	S. 047 = 305' = 370'
④ 1.389 - 7°	1.389	7.117	L. 017 = 1075+1035
⑤ 5.120 - 12°	4.769	11.586	L. 030 = 1075+1035
⑥ 0.530 - 15°	.489	12.675	L. 030 = 1075+1035
⑦ .061 -	.061	12.736	L. 20' R. 007 = 5.113
⑧ 1.204 - 36°	.969	13.705	S. 122 = 743' 700'
⑨ 3.652 - 34°	3.028	16.733	L. 17.30' = 5.147
⑩ .880 -	.880	17.613	L. 2.30' = 7.015
⑪ 2.463 - 30°	2.122	19.735	S. 179 = 145' 18.77
.122	.122	19.857	S. 180 = 147' 14.99
		143	
		20.000	Set Stake.

Angle at Vertex of Δ 3°21½' Distance 68.313

④	7.117	Point
⑤ 68.313	68.313	Point
.630 -	7.5430	
	76.860	
4.855 - 90°	4.795	80.855
2.247 - 88°	2.222	83.077
	1.17	
	82.960	
	1.43	
	83.103	Falls .689 S. of 7500. cor.

This is the original post and was not re-established
as per J.A.G. Fic B.T. is N. 88°40' E. Not 87°40' as per map

272° 20 21 340° 29.53
237° 76 365 270 28
2.097

413° 20
3° 21½

17.813 30.2 20.61
14.1 54
17.756 2463 2122
2122
17.877

A. Skaggs

Calc 1 11.23 25837
4.078 0.61 04479
11.35 9.99 25492
68483 21.83 53 794
Calc 2 11.0230 4226
0.61 14474
99.92 5492
68453
21.833 4183
68313

99.74
38
37
1171
30' 7940842
45509129419
207415 17.870261
30' 7940842
38 9.944483
207415 17.875325
99.9940871
9.9444835
9.9994677
29.8380374
68.7
93.103
7.918420
28' 30"